DLR TAU Simulations for the Second AIAA Sonic Boom Prediction Workshop

Jochen Kirz and Ralf Rudnik

German Aerospace Center (DLR), Institute of Aerodynamics and Flow Technology AIAA Aviation, June 05, 2017



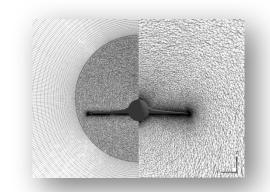


Outline

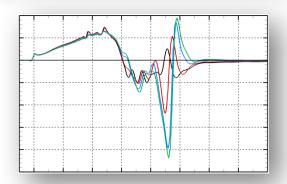
- Motivation and Background
- SBPW2 Configurations and Grids
- Flow Solver and Computing Platform

Simulation Results and Data Comparison

Summary, Conclusions and Outlook



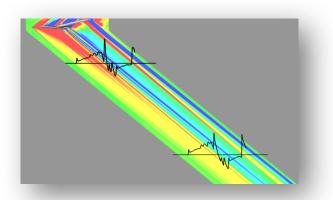






Motivation and Background

- Considerable market for supersonic aircraft
- Certification of a low boom aircraft to fly supersonically over land would allow new routes



- AIAA Sonic Boom Prediction Workshop intends to assess the state of the art for predicting near-field pressure signatures, ground signatures and perceived loudness levels
- DLR did not upload data for the first SBPW (January 2014) but participated as an observer
- In early 2016 DLR started to use the available data from SBPW1 to build a best practice for near-field pressure signature prediction with the DLR TAU code
- DLR uploaded near-field pressure signatures for SBPW2 and participated in January 2017



SBPW2 Configurations

Overview





Axisymmetric body

 Matching the pressure signature of C25F at 3 body lengths



JWB

JAXA delta wing body

 Same equivalent area as the C25D



NASA C25D

Full configuration with tail

- C25F: flow-through nacelle
- C25P: powered engine

Available Data

- Geometries and grids
- Pressure signatures from other participants

Simulation Conditions

- M = 1.6
- H = 15760 m
- T = 216.65 K
- $Re = 5.7 \cdot 10^6 / m$



Cases Analyzed and Grids Used

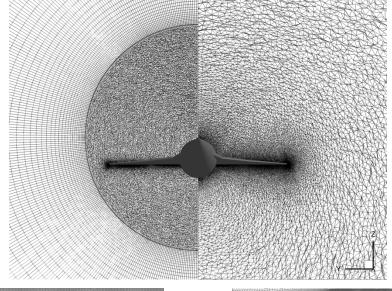
AXIE-inv	JWB-inv	C25F-inv	C25F-visc	C25P-inv
WS-mixed, h=4.42		WS-mixed, h=2.00	WS-mixed, h=2.00	WS-mixed, h=2.00
WS-mixed, h=3.27		WS-mixed, h=1.60		WS-mixed, h=1.60
WS-mixed, h=2.23		WS-mixed, h=1.28	WS-mixed, h=1.28	
WS-mixed, h=1.52		WS-mixed, h=1.00	WS-mixed, h=1.00	WS-mixed, h=1.00
		WS-mixed, h=0.80	WS-mixed, h=0.80	WS-mixed, h=0.80
		WS-mixed, h=0.64		
WS-tet, h=4.42	WS-tet, h=1.00	WS-tet, h=2.00	WS-tet h=2.00	
WS-tet, h=3.27	WS-tet, h=0.83	WS-tet, h=1.60		
WS-tet, h=2.23	WS-tet, h=0.70	WS-tet, h=1.28	WS-tet h=1.28	
WS-tet, h=1.52		WS-tet, h=1.00	WS-tet h=1.00	
CENT-mixed	CENT-mixed, h=1.68	CENT-mixed, h=1.00		
	CENT-mixed, h=1.00			
	CENT-mixed, h=0.81			
	CENT-mixed, h=0.65			

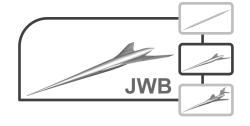


Grids JWB

CENTAUR-generated

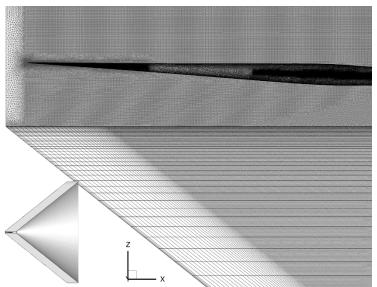
- Core grid➤ Tetrahedra
- Collar grid➤ Hexahedra

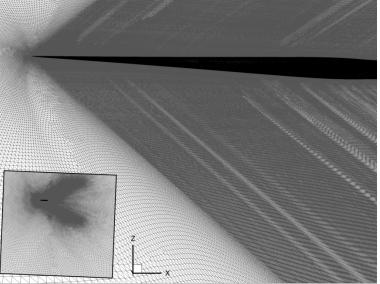




Workshop-provided

Purely tetrahedral



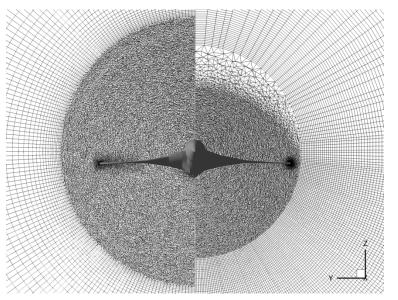


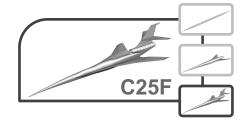


Grids C25F

CENTAUR-generated

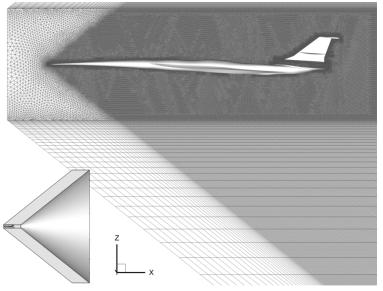
- Core grid➤ Tetrahedra
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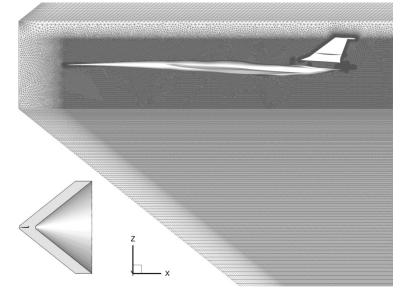




Workshop-provided

- Core grid➤ Tetrahedra
- Collar grid
 Prisms/
 Tetrahedra





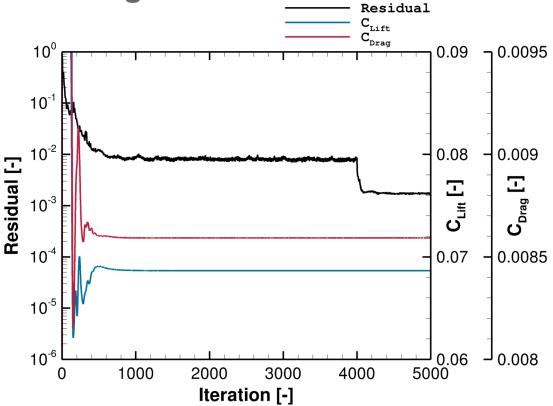


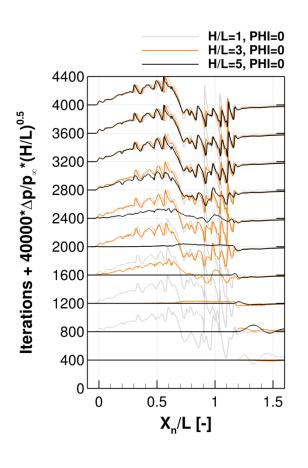
Flow Solver and Computing Platform

- DLR TAU Code
 - Unstructured finite-volume
 - Euler, RANS
 - Hybrid grids
 - Backward Euler and Runge-Kutta timestepping
 - Central and upwind schemes (Roe, Van Leer, AUSMDV, AUSMP(W+))
 - 2nd order upwind limiter functions (Barth Jesperson, Venkatakrishnan, SRR)
- C²A²S²E-2 Cluster
 - 1 computing node (24 cores) per 300.000 grid nodes





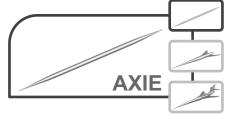


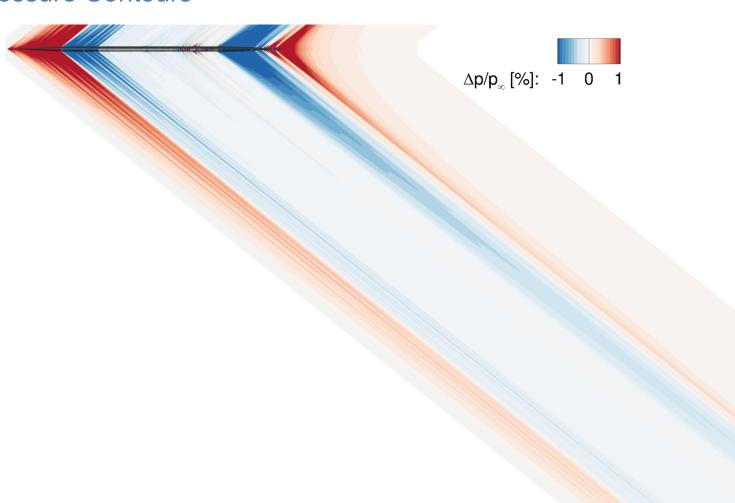


- **CFL Ramping**
- Aerodynamic coefficients converged at 1000 iterations
- Pressure signatures in the farfield converged significantly later
- Convergence criteria:

5000 Iterations (inviscid simulations) / 15000 iterations (viscous simulations)

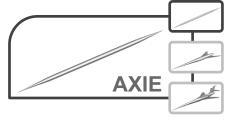
Pressure Contours

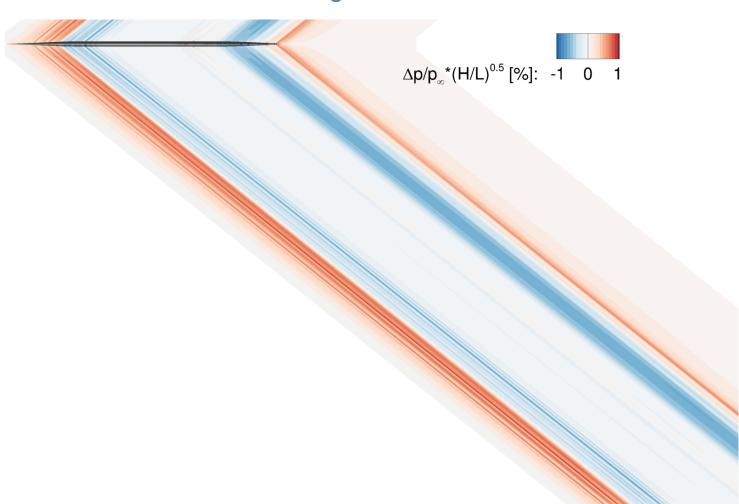






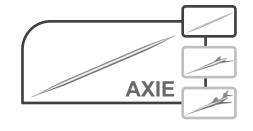
Normalization and Pressure Signature Extraction

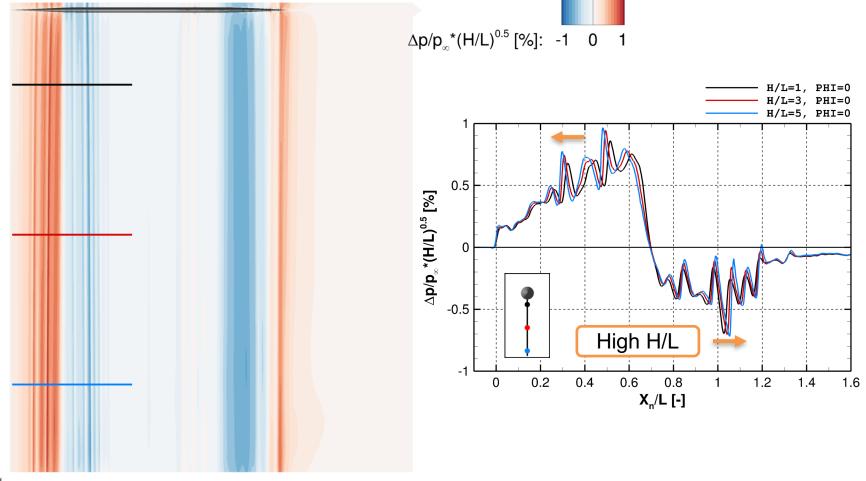






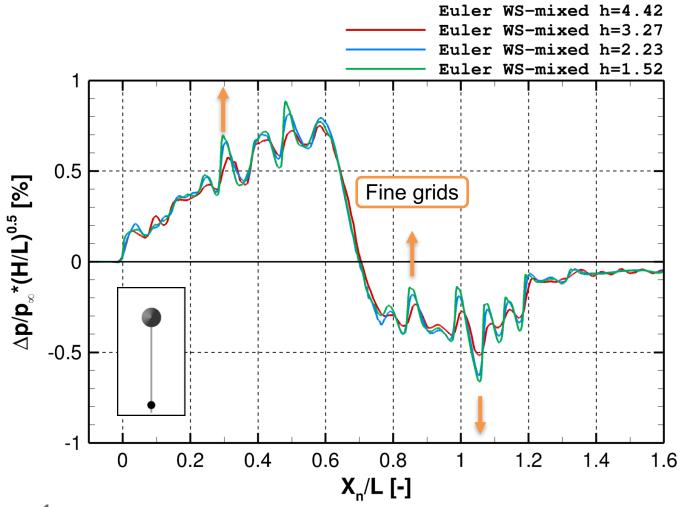
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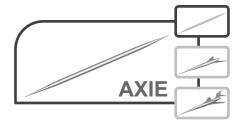






Pressure Signature Convergence (H/L=5, PHI=0)

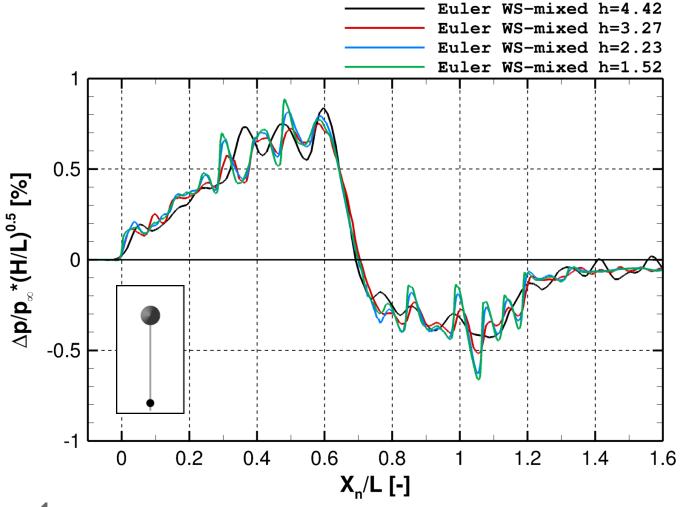


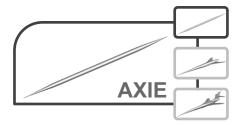


- Positions of shocks and expansions coincide for medium to fine grids
- Magnitudes are larger on fine grids (less dissipative)



Pressure Signature Convergence (H/L=5, PHI=0)

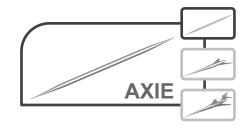


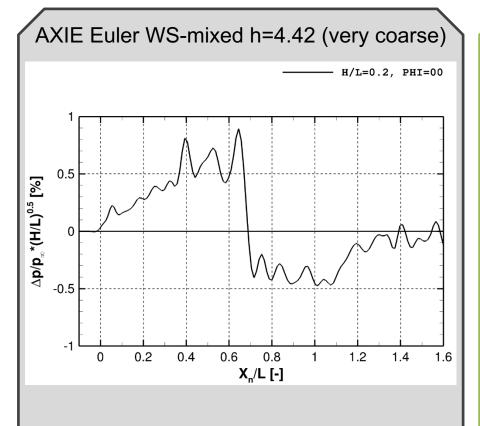


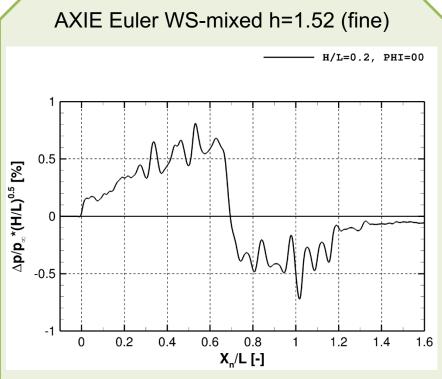
- Positions of shocks and expansions coincide for medium to fine grids
- Magnitudes are larger on fine grids (less dissipative)
- Positions of shocks and expansions differ for very coarse grids



Mesh-Induced Pressure Disturbances

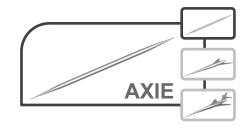


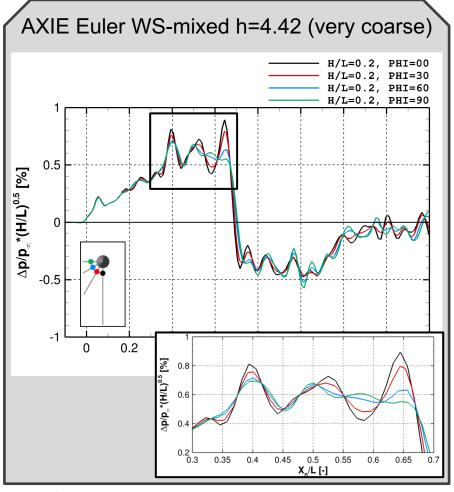


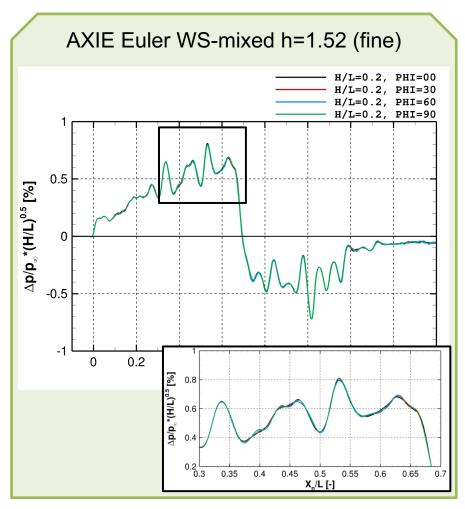




Mesh-Induced Pressure Disturbances

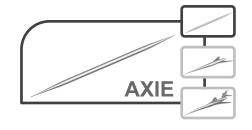


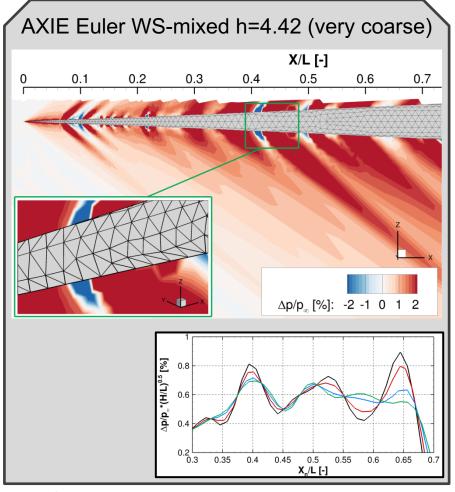


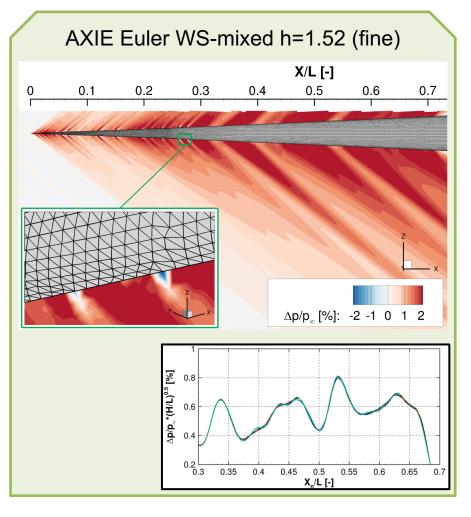




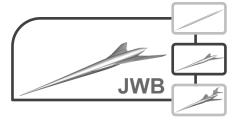
Mesh-Induced Pressure Disturbances







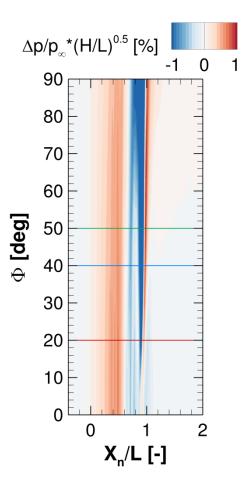


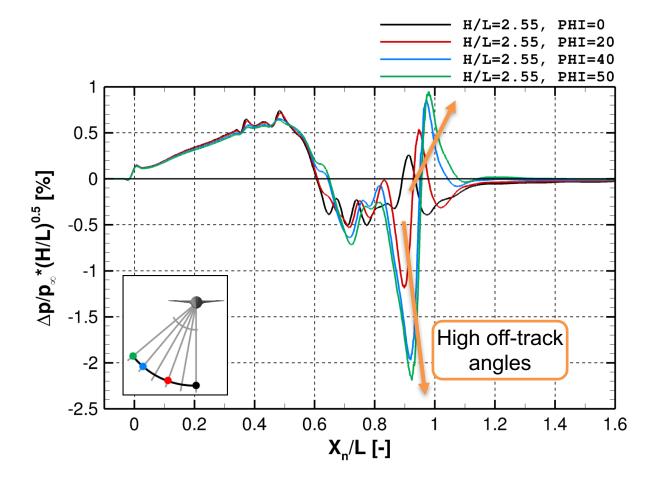




Pressure Contours and Near Field Signatures







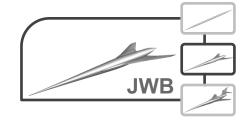


Pressure Signature Convergence (H/L=2.55, PHI=0)

Euler WS-tet h=1.00

Euler WS-tet h=0.83

Euler WS-tet h=0.70



8.0 0.4 ∆p/p_∞*(H/L)^{0.5} [%] 0 -0.4 -0.8 0.2 0.4 0.6 0.8 1.2 1.4 1.6 X_n/L [-]

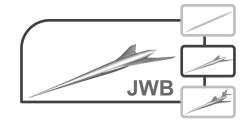
WS-provided grids

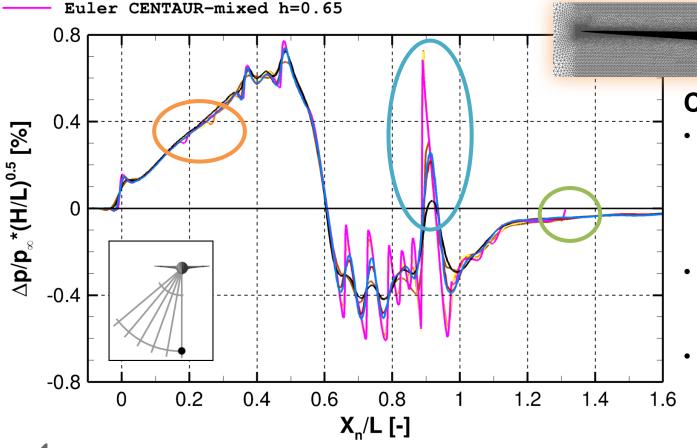
- Positions of shocks and expansions coincide
- Signature convergence with grid refinement



Pressure Signature Convergence (H/L=2.55, PHI=0)

Euler CENTAUR-mixed h=1.68 — Euler WS-tet h=1.00 Euler CENTAUR-mixed h=1.00 — Euler WS-tet h=0.83 Euler CENTAUR-mixed h=0.81 — Euler WS-tet h=0.70





CENTAUR grids

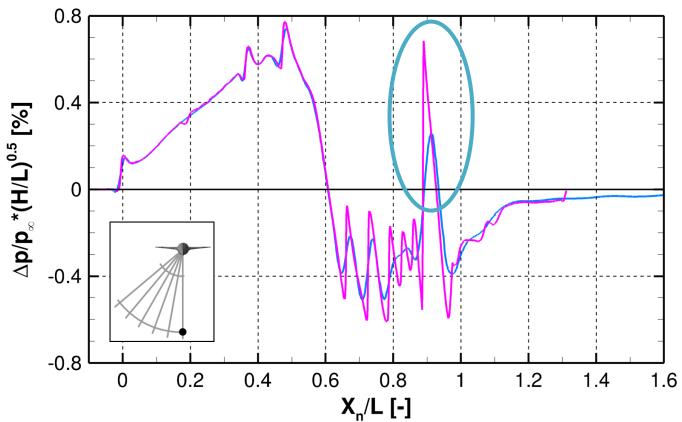
- Mesh-induced pressure disturbances at the nose
- Lower streamwise extent
- Larger magnitudes at tail shock



Pressure Signature Convergence (H/L=2.55, PHI=0)

Euler CENTAUR-mixed h=1.68 Euler CENTAUR-mixed h=1.00 Euler CENTAUR-mixed h=0.81 Euler WS-tet h=1.00 Euler WS-tet h=0.83 Euler WS-tet h=0.70

Euler CENTAUR-mixed h=0.65





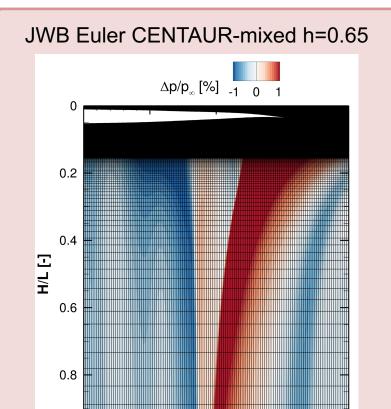
CENTAUR grids

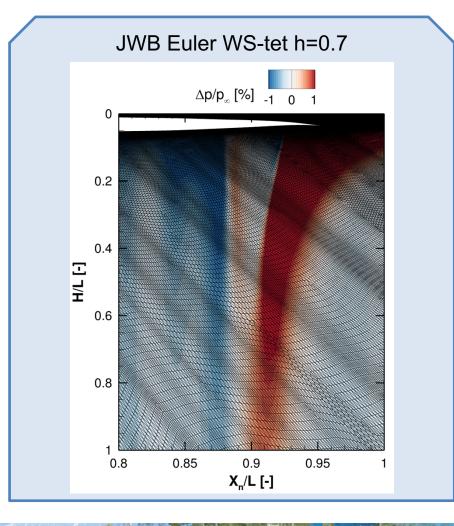
- Mesh-induced pressure disturbances at the nose
- Lower streamwise extent
- Larger magnitudes at tail shock



Smoothing of the Pressure Signature (Symmetry Plane)









0.8

0.85

0.9

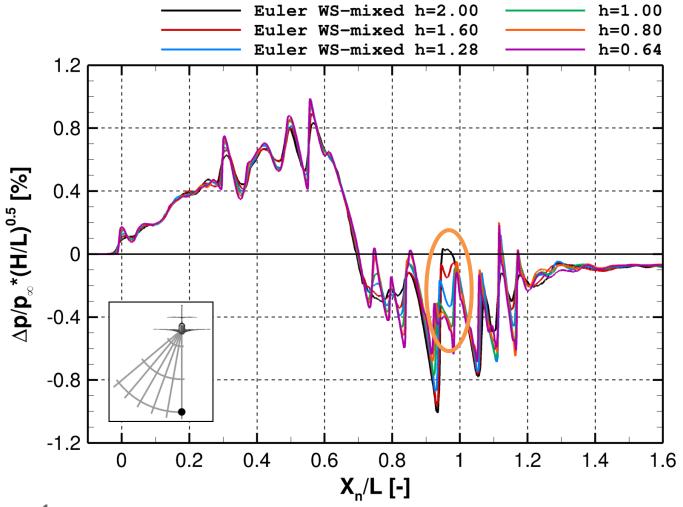
 X_n/L [-]

0.95





Pressure Signature Convergence (H/L=5, PHI=0)

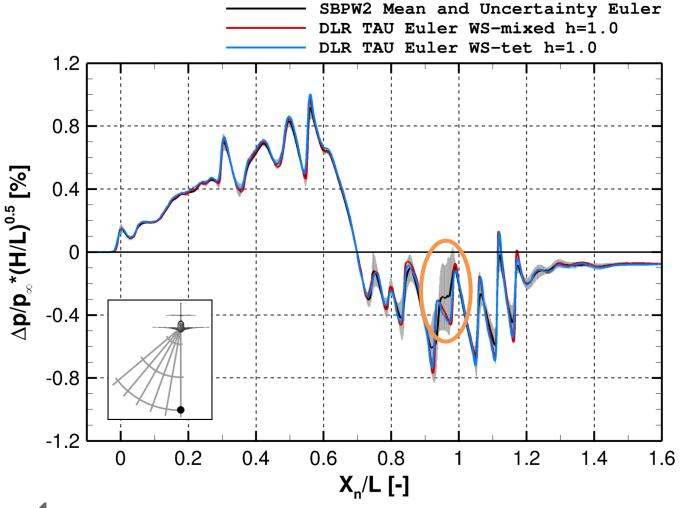




- Large differences at $0.9 < \frac{X_N}{L} < 1$
- Reflections of nacelle leading edge shock on the upper wing and lower HTP surfaces
- Grid convergence for h<1.00



TAU Signatures and SBPW2 Statistics (H/L=5, PHI=0)

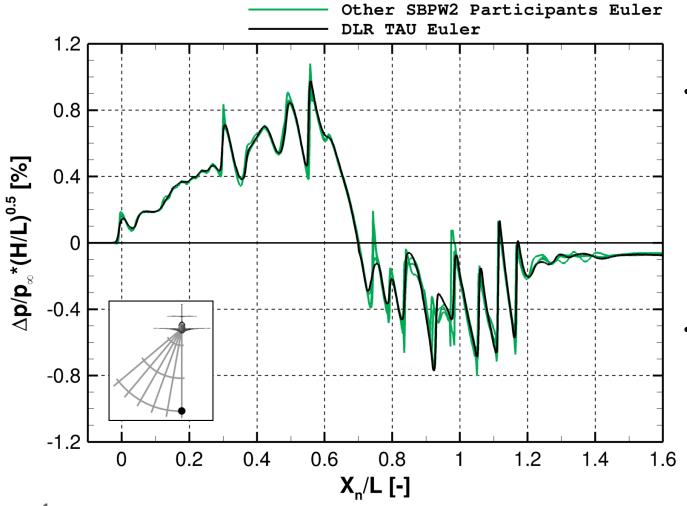


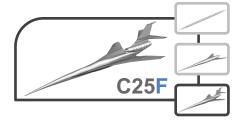


- Pressure signatures for fine mixed-element and fine purely tetrahedral grid very similar
- Both match the workshop mean well
- Differences at the reflections of the nacelle leading edge shock due to averaging



Same Grid Comparison (H/L=5, PHI=0)

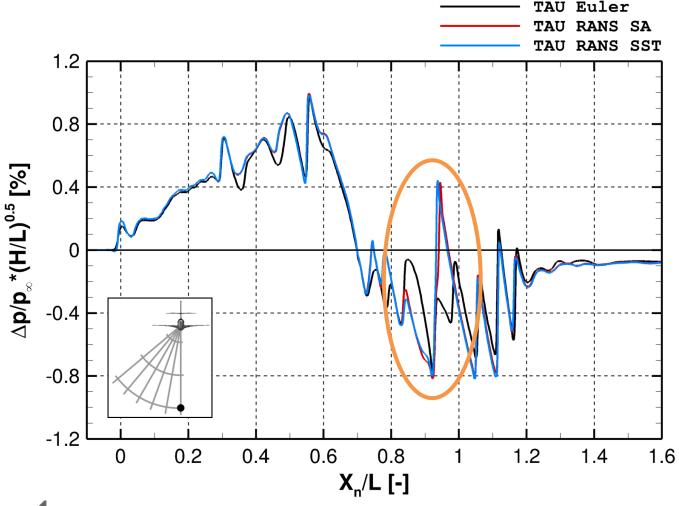




- Pressure
 magnitudes slightly
 lower for TAU code
 compared to other
 participants'
 pressure
 signatures on the
 same grid
- Positions of shocks and expansions in good agreement



Euler and RANS Simulations (H/L=5, PHI=0)

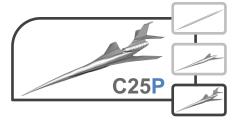




- Small influence of turbulence model
- Larger pressure
 magnitudes at
 initial compression
 for RANS
 simulations due to
 effective thickening
 of the body
 through the
 boundary layer
- Significant differences at nacelle inlet shock reflections



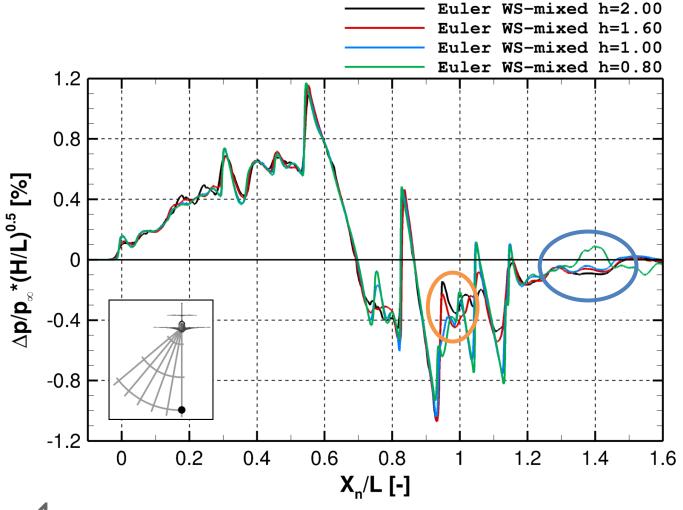
Results C25D powered





Results C25D powered

Pressure Signature Convergence (H/L=5, PHI=0)



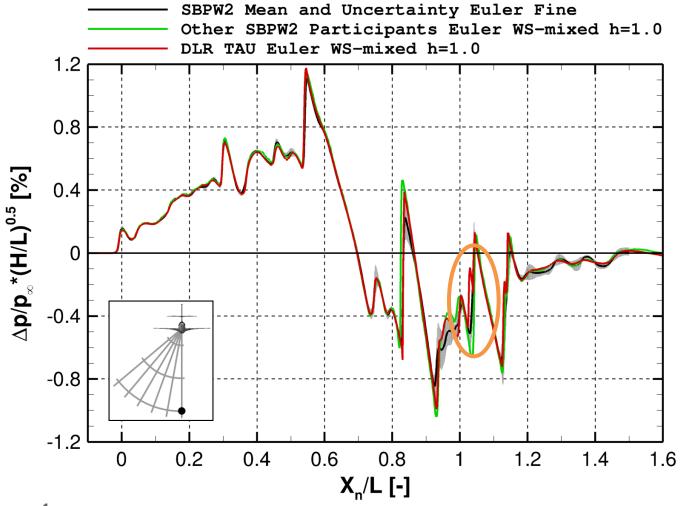


- Largest differences at nacelle inlet shock reflections
- Similar to the C25F
- Artificial compression due to grid coarsening in the plume



Results C25D powered

TAU Signatures and SBPW2 Statistics (H/L=5, PHI=0)





- TAU pressure signature matches the workshop mean
- Slight differences at engine outlet



Summary and Conclusions

- Euler and RANS simulations performed with the DLR TAU code for 38 workshop-provided and CENTAUR-generated grids
- Positions of shocks and expansions
 - Similar for grids with medium to fine resolution
 - Different for very coarse grids
- Pressure magnitudes at shocks and expansions
 - Higher for fine grids compared to coarse grids (less dissipative)
 - Higher for purely tetrahedral grids compared to mixed-element grids
- Fine grids needed to capture reflections of C25D nacelle LE shock
- Influence of viscosity larger than influence of grid setup
- TAU pressure signatures in good agreement to results of other codes
- → Best-practice for near-field prediction with the DLR TAU code improved
- → Robust and fast pressure signature prediction for simplified as well as complex cases



Outlook

- Improving best-practice for mesh generation for viscous simulations
- Ground propagation and ground loudness calculation
- Design and optimization of a supersonic configuration towards low boom low drag

Acknowledgements

 Committee of the AIAA Sonic Boom Prediction Workshops for providing geometries, grids and statistical data



Backup Slides

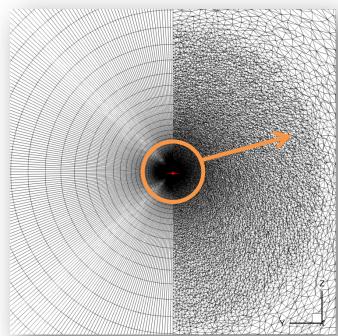


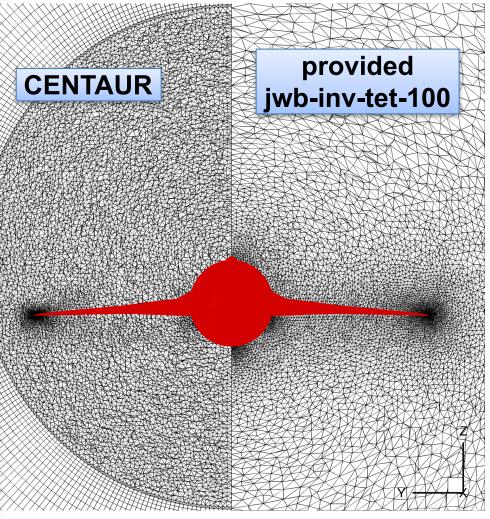


Cases Analyzed and Grids Used

CENTAUR-generated Grids for JWB case

- Hybrid Euler grids
 - Unaligned tetrahedrons in cylindrical inner part
 - Mach cone aligned hexahedrons in farfield

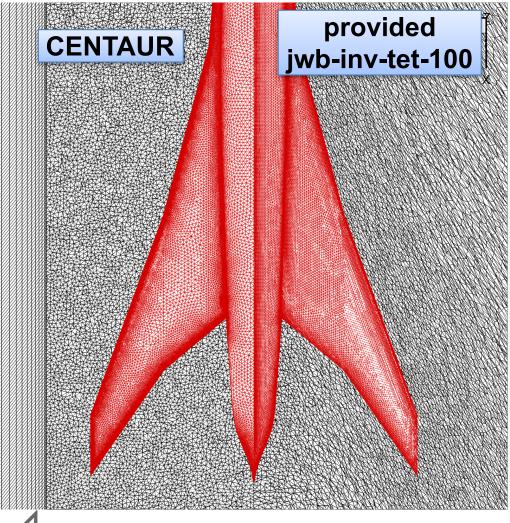




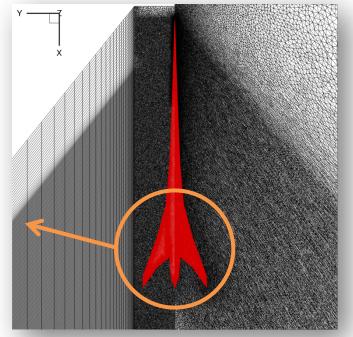


Cases Analyzed and Grids Used

CENTAUR-generated Grids for JWB case



 Surface resolution (triangles) of coarse CENTAUR grid similar to coarse workshop-provided grid



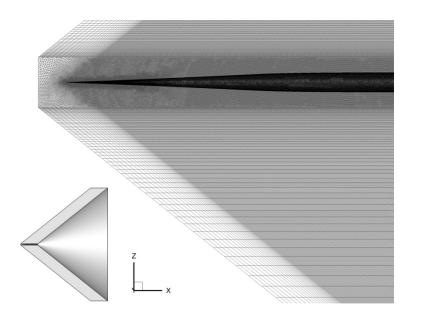


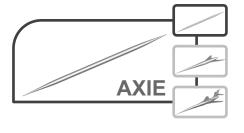
Grids

AXIE

CENTAUR-generated

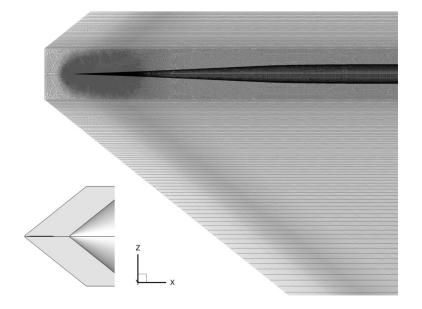
- Core grid
 - > Tetrahedra
- Collar grid
 - > Hexahedra



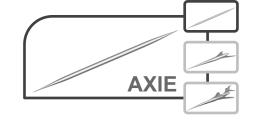


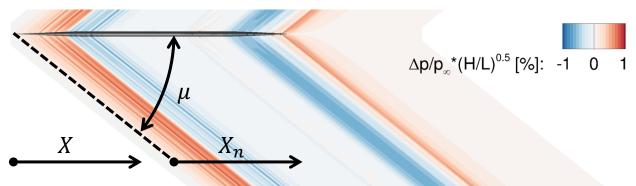
Workshop-provided

- Core grid
 - > Tetrahedra
- Collar grid
 - ➤ Prisms/ Tetrahedra

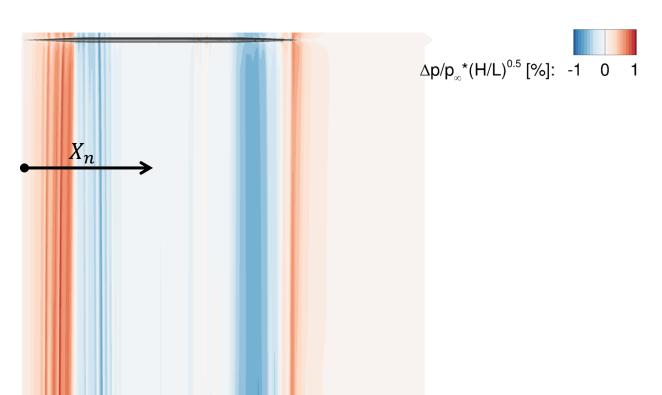


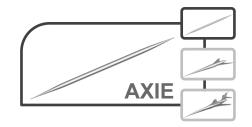




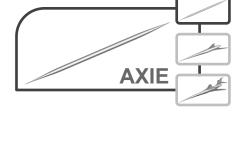


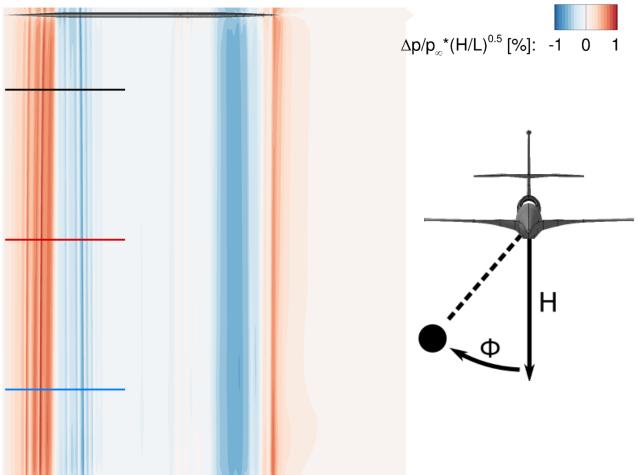




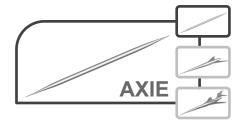


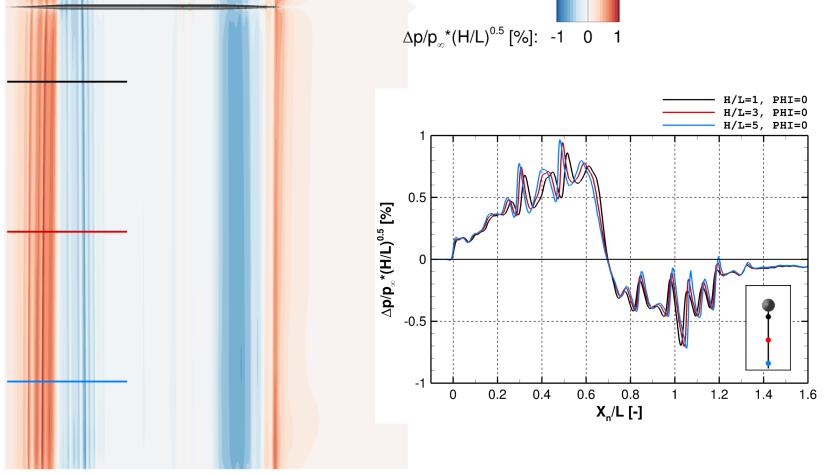






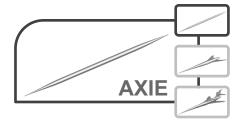


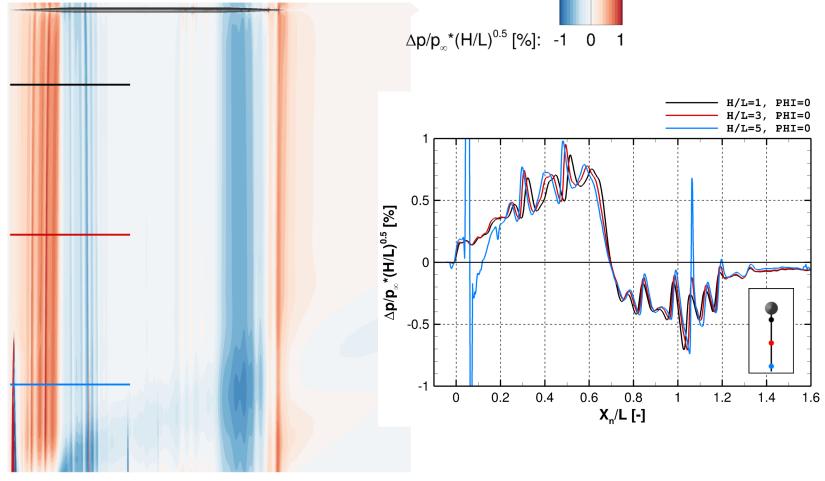






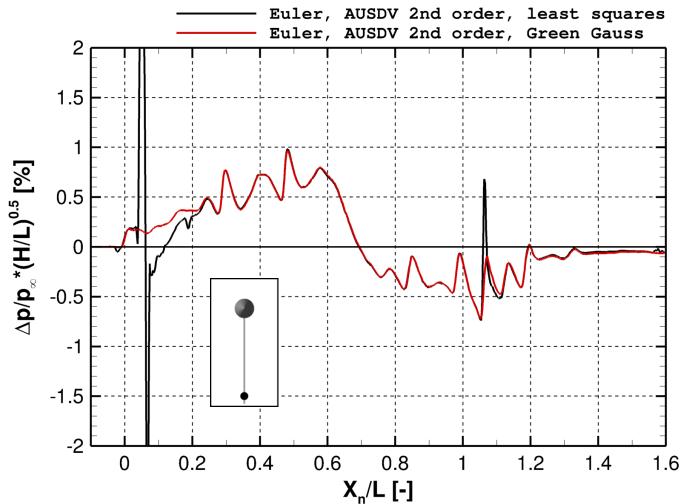
Least Squares Reconstruction of Gradients

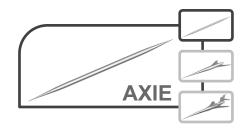






Least Squares vs Green Gauss







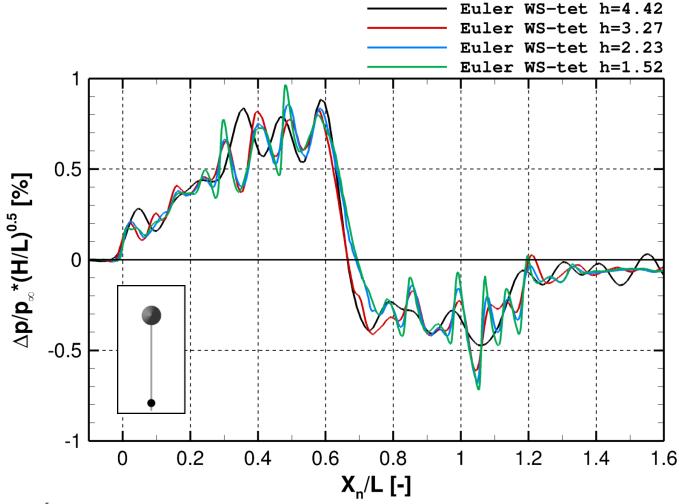
Highlights

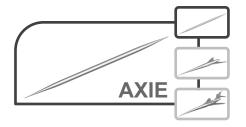
Inflow and Farfield Boundary Condition Changes

- Supersonic inflow/outflow
 - Compute boundary fluxes with approximate Riemann solver instead of setting conservative variables at the boundary
 - The gradients of all variables are set to zero in the direction normal to the boundary
- Farfield
 - The farfield fluxes are evaluated via a characteristic method that is in line with the interior face-flux computation.
 - The corresponding flux parameters are inherited from the central, matrix-dissipative scheme
- Convergence improved as side effect (more robust start, significantly less iterations needed and residual lowered by 1-2 orders of magnitude)



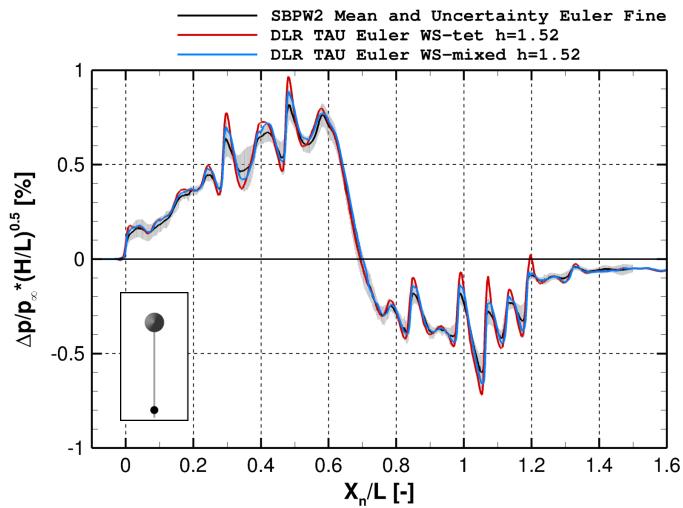
Pressure Signature Convergence (H/L=5, PHI=0)

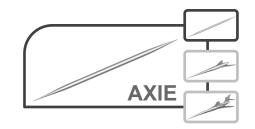




- Positions of shocks and expansions coincide for medium to fine grids
- Magnitudes are larger on fine grids (less dissipative)

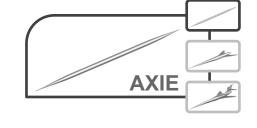


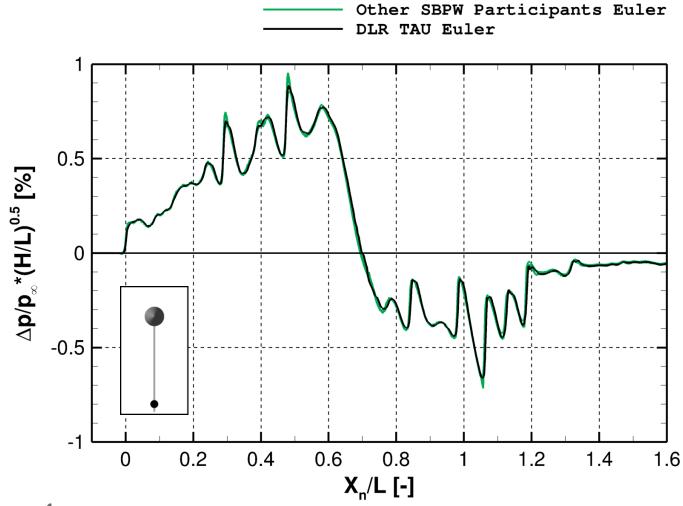






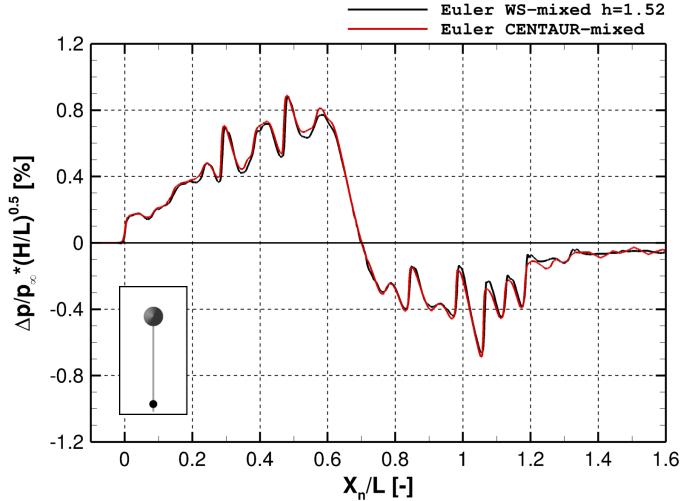
Same grid

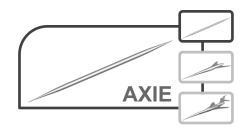




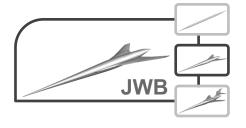


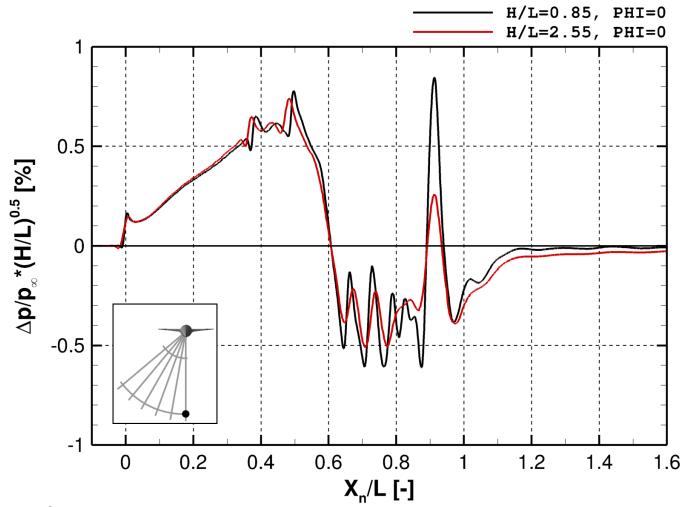
Provided and CENTAUR-generated grid





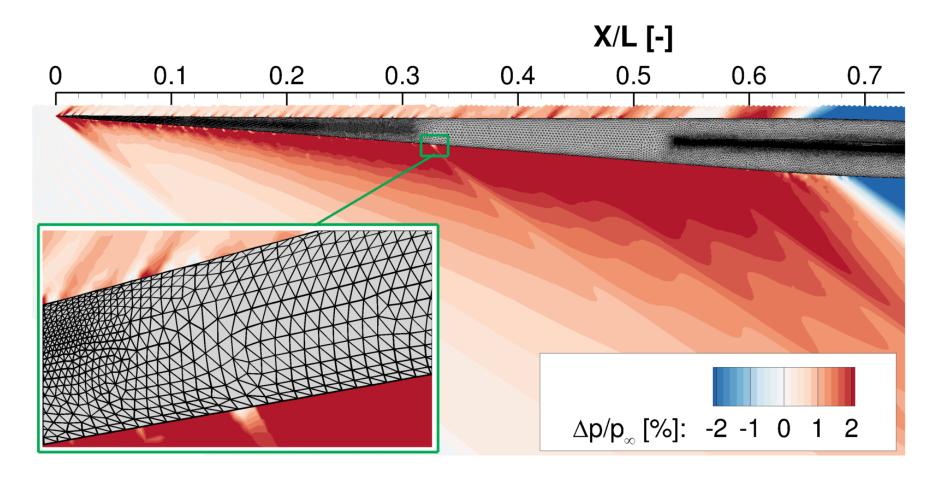




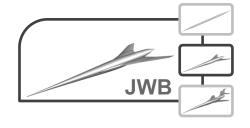


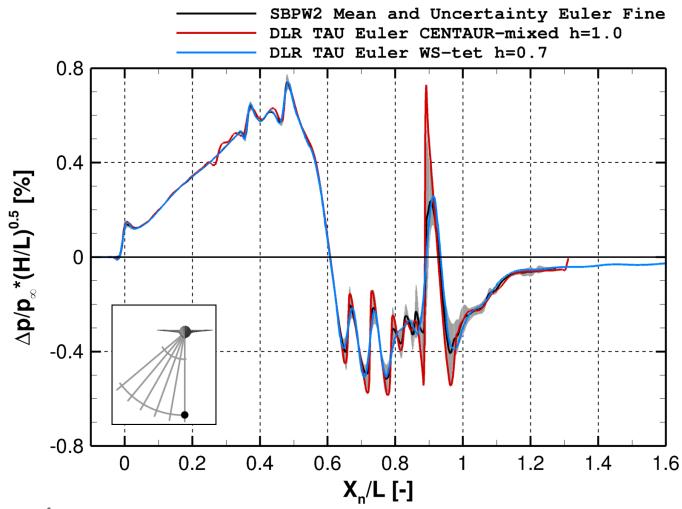




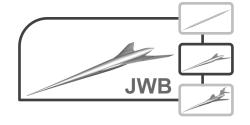


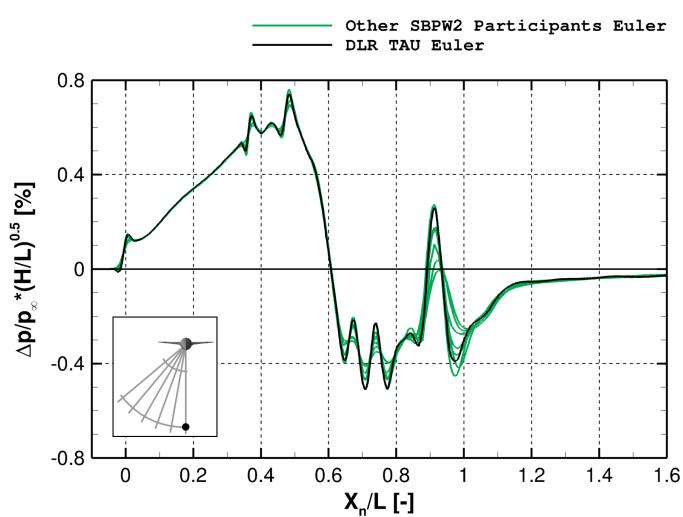






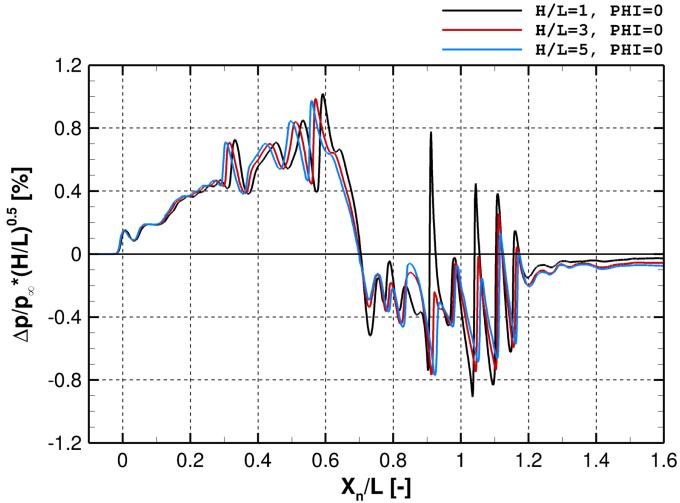


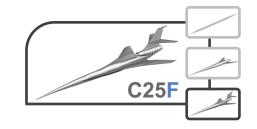






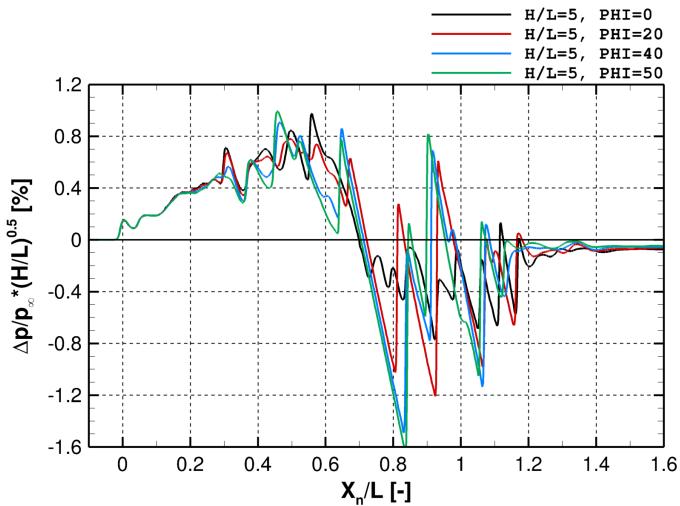
On-track Pressure Signatures (PHI=0)

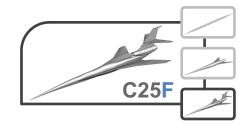




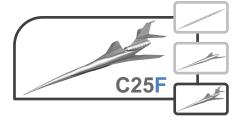


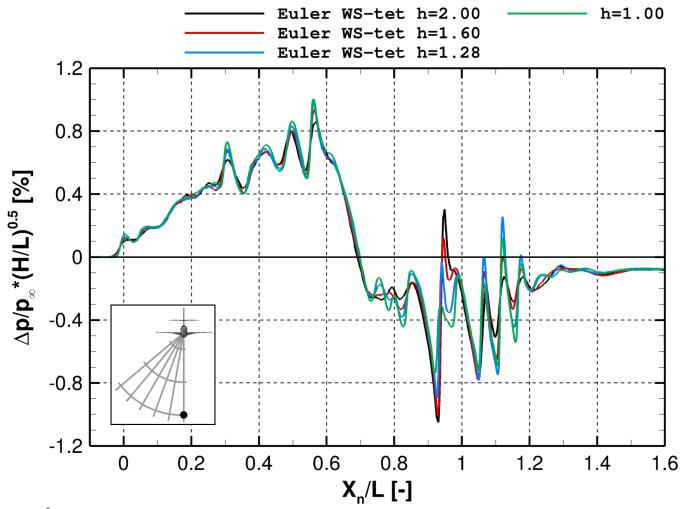
Off-track Pressure Signatures (H/L=5)



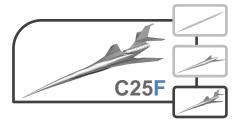


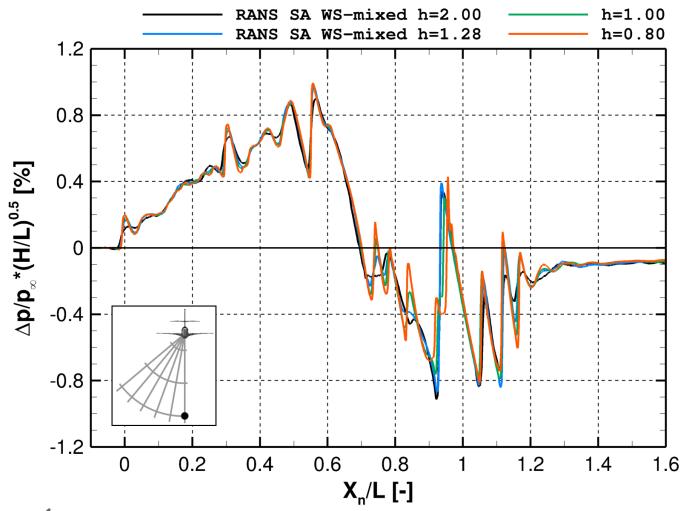




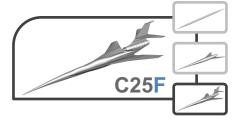


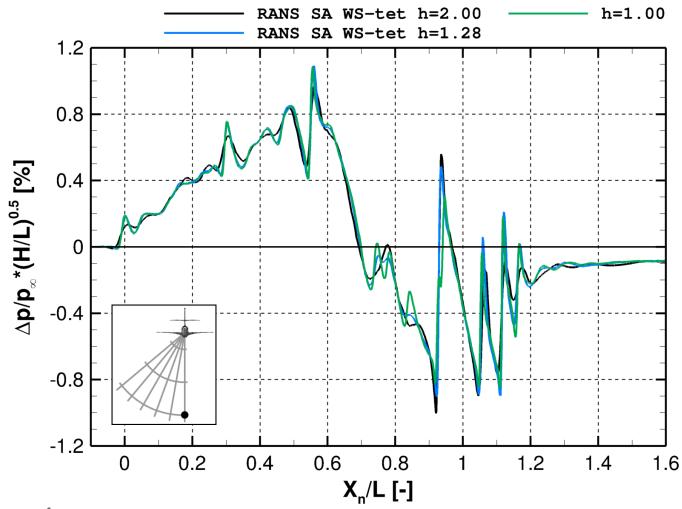




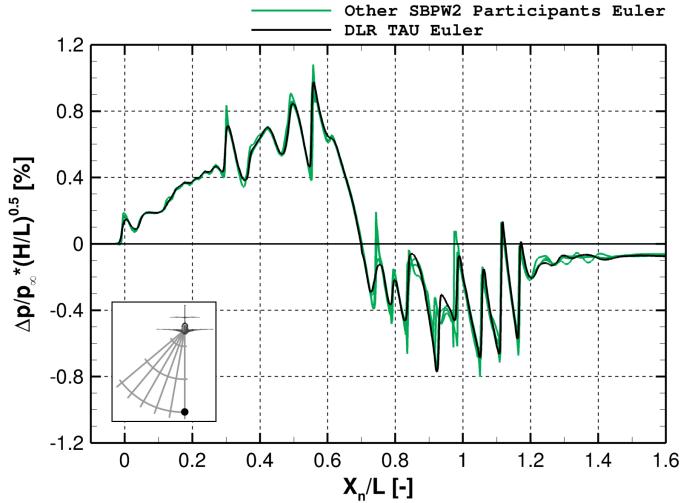






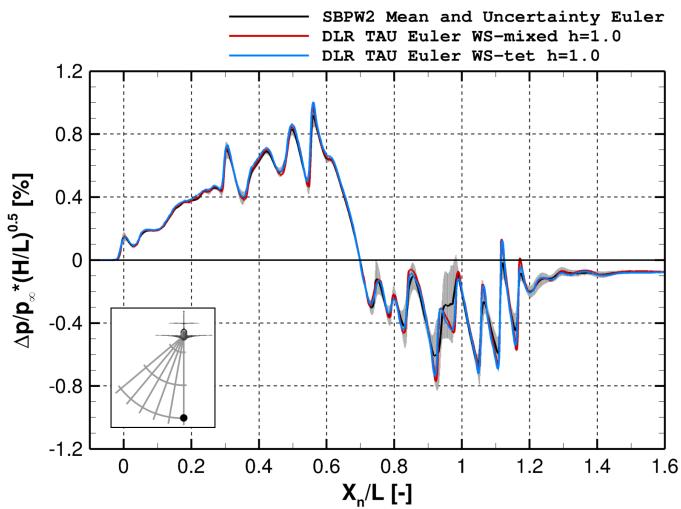


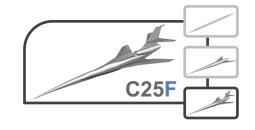




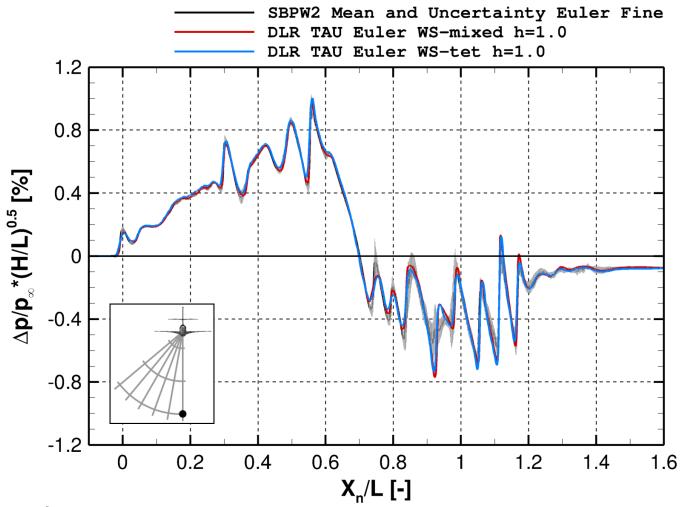


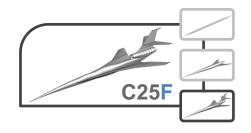




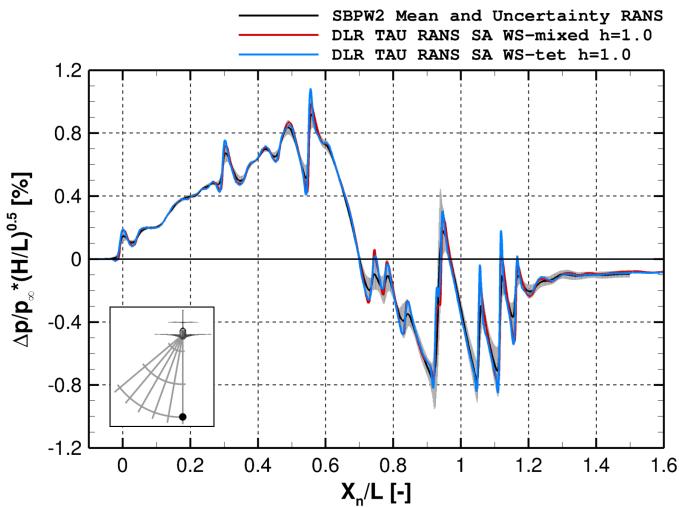


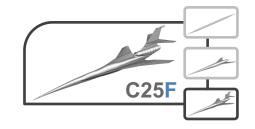




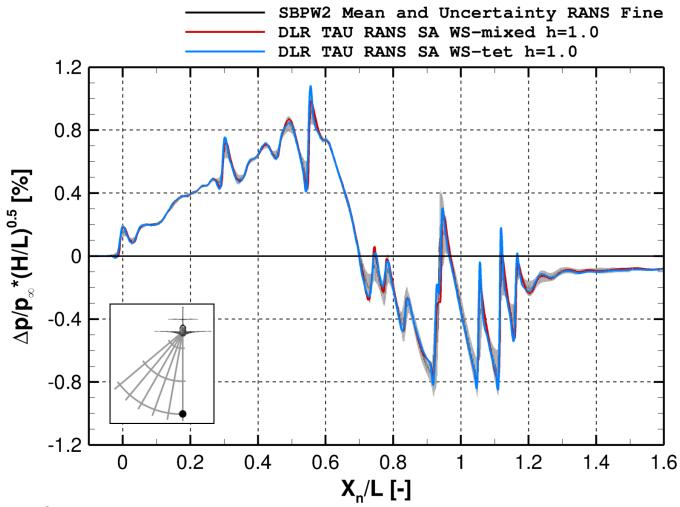


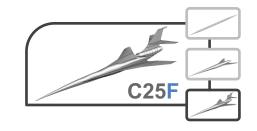




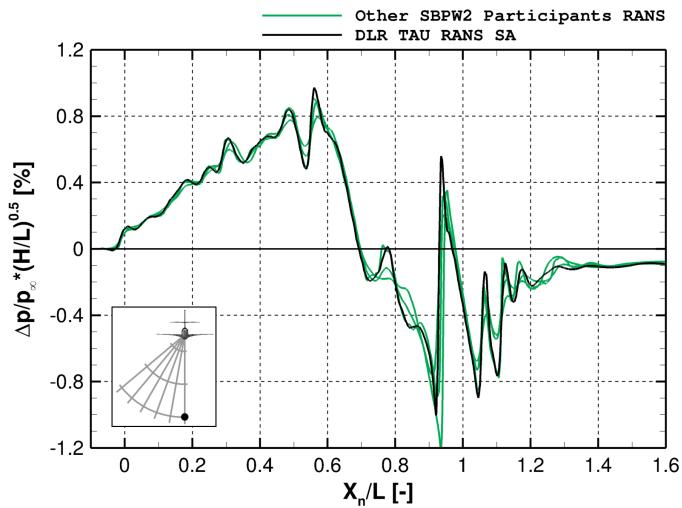


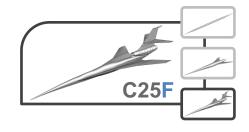




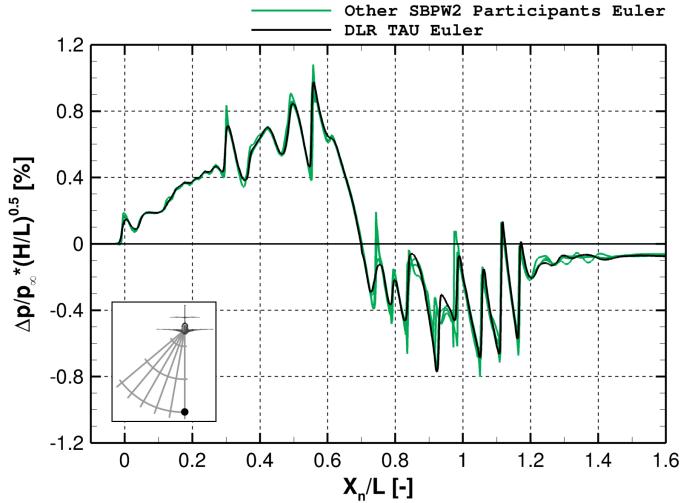


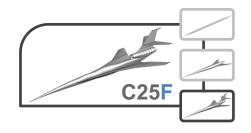




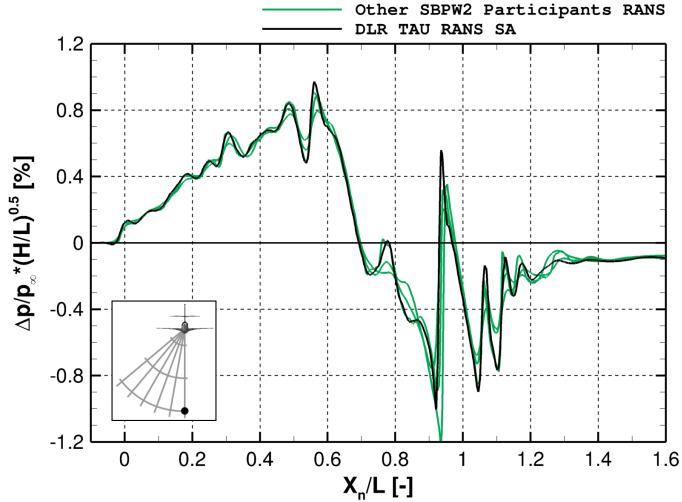


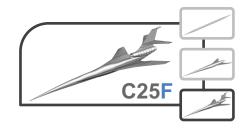






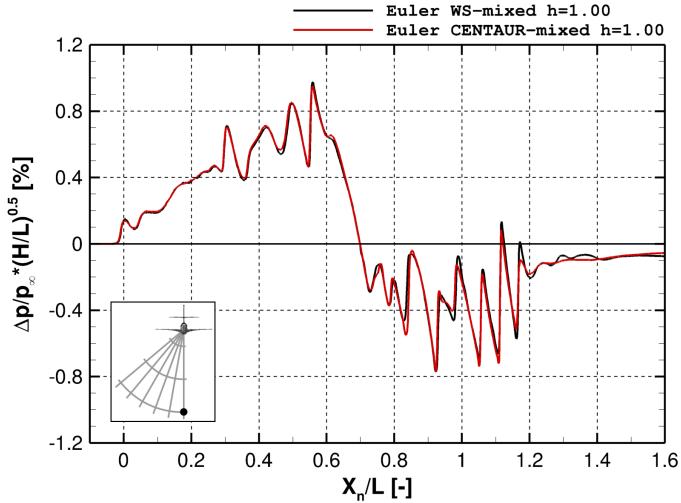








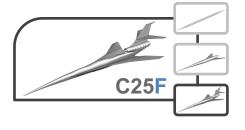
Provided and CENTAUR-generated grid

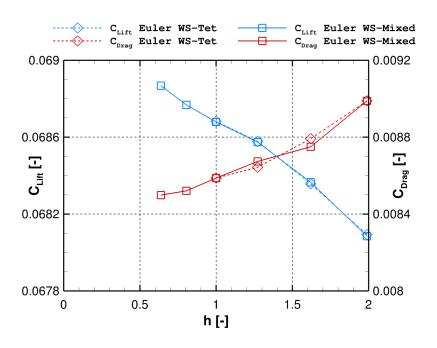


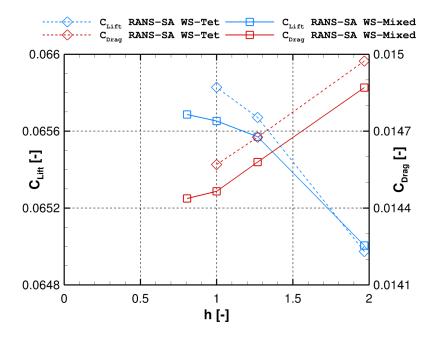




Forces









Results C25D powered

